

1 **Online Resource 1 for:**

2 **Aging and the effects of a half marathon on Achilles tendon force-elongation**
3 **relationship.**

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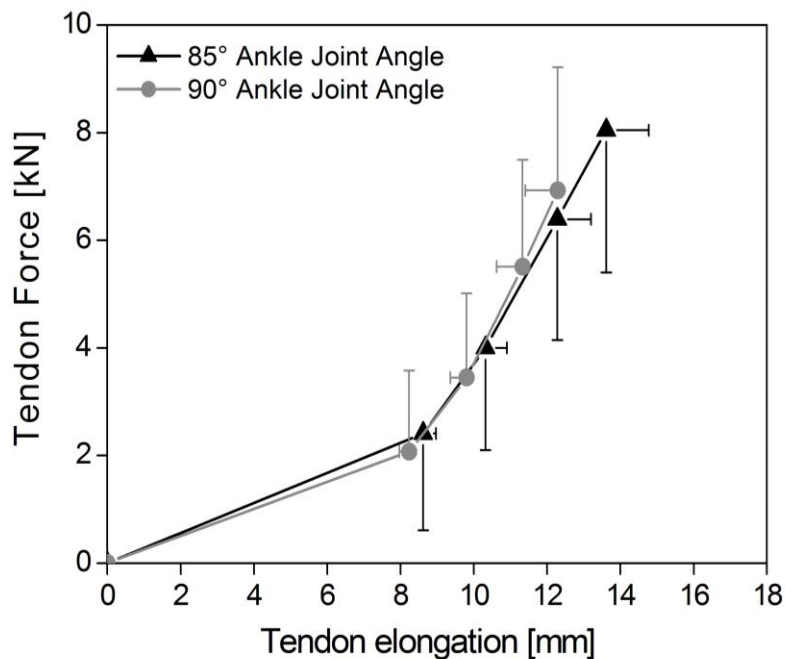
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14 **Methodological Considerations and Pilot Data**

15 Before conducting the current study we performed several pilot studies in order to test
16 the accuracy of the current method to examine the mechanical properties of the AT.

17 While a 90 degree knee position, with more secure fixation of the limb, may result in
18 much less ankle joint angular rotation than straight knee set ups (average changes of
19 14-18 degrees at the ankle joint have been reported when using a fully extended knee;
20 see e.g.: Arampatzis et al., 2005; Karamanidis et al., 2005), examining the force-
21 elongation relationship of the tendon in this way could potentially place the GM in a
22 less favorable position on the force-length relationship, when compared to a fully
23 extended knee. This might be problematic, since we calculated the net joint moment
24 at the ankle joint, but measured the elongation of the GM tendon. Moreover, the AT
25 cannot be considered as a single tendon that extends uniformly during plantarflexor
26 contractions, which might lead to an erroneous calculation of the stiffness in absolute
27 terms. In order to address this drawback we conducted a pilot study using a more
28 dorsiflexed ankle joint position (85 degrees ankle joint angle). As a result we
29 lengthened the entire TS MTU and in particular, tensed the GM tendon, causing a
30 rightwards shift in the force-length relationship of the contractile element of the
31 *gastrocnemii*. This increased its force potential and hence the contribution of the GM
32 to the net joint moment (Arampatzis et al., 2006). In this pilot study, with 10 healthy

33 subjects, we compared an ankle angle of 90 degrees to the dorsiflexed ankle joint
34 angle of 85 degrees. An ankle angle of 90 degrees resulted in a significantly ($P <$
35 0.05) lower ankle joint moment (90 degrees: $277 \pm 35 \text{ N}\cdot\text{m}$ vs. 85 degrees: 322 ± 46
36 $\text{N}\cdot\text{m}$; mean and SD) and maximal tendon elongation (90 degrees: $12.3 \pm 2.3 \text{ mm}$ vs.
37 85 degrees: $13.6 \pm 2.8 \text{ mm}$) compared to a dorsiflexed ankle joint angle of 85 degrees.
38 However, there was no significant difference in tendon stiffness between the two
39 setups (85 degrees: $1219 \pm 461 \text{ N}\cdot\text{mm}^{-1}$ vs. 90 degrees: $1210 \pm 283 \text{ N}\cdot\text{mm}^{-1}$; see Fig
40 S1). Therefore, while a flexed knee joint reduces *triceps surae* force generation
41 capacity, and the contribution of the gastrocnemii to this force potential (decreasing
42 total tendon lengthening) and, in addition, might place the GM tendon in more slack
43 position, it appears not to lead to changes in the force-length relationship of the
44 tendon during loading.
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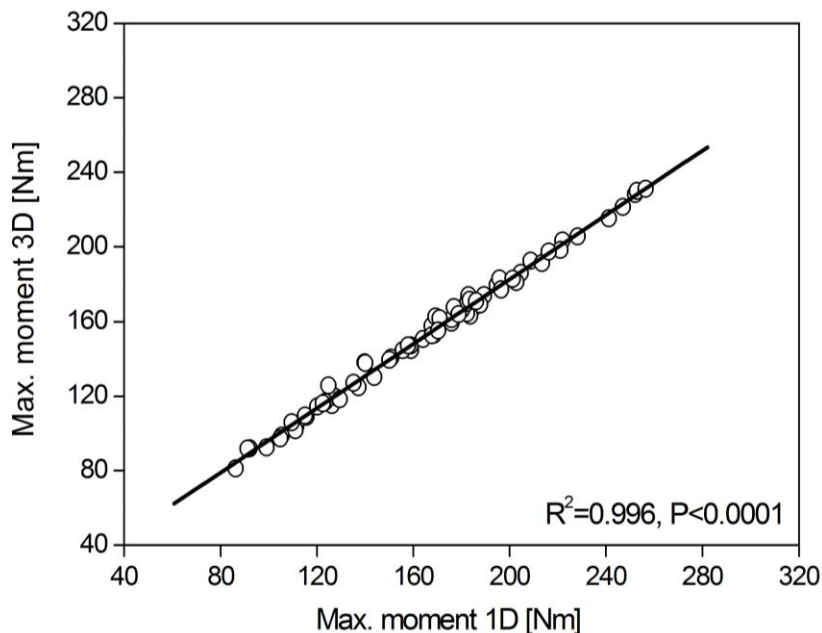
58 **Fig S1** Force-length relationship (mean and SD) of the tendon measured with an ankle joint angle of 90
59 degrees (foot perpendicular to the shank) and a more dorsiflexed angle of 85 degrees, each with a knee
60 joint angle of 90 degrees (thigh perpendicular to shank), for 10 healthy young subjects. No significant
61 differences in force-elongation relationship of the tendon were found when comparing the ankle joint
62 angles (tendon stiffness at 85 degrees: $1219 \pm 461 \text{ Nmm}^{-1}$ vs. tendon stiffness at 90 degrees: $1210 \pm$
63 283 Nmm^{-1}).

64 In a second pilot study, with nine healthy subjects, we compared ankle joint angle
65 changes during isometric contractions estimated using different calculation methods.
66 The ankle joint angle changes in the sagittal plane (2D analysis), calculated by inverse
67 kinematics using reflective markers fixed at the lower extremity of the subjects
68 acquired by a motion capture system (120Hz, Qualisys, Gothenburg, Sweden)
69 together with a force plate (1080 Hz, 400 x 600 mm, Bertec, Columbus OH, USA),
70 were compared to the method used in the current study that estimated ankle joint
71 angle changes based on data from a potentiometer located under the heel (current
72 method). The potentiometer used in the current study measured any heel elevation and,
73 thereby, calculated changes in the ankle joint angle from rest until maximal (Fig. 1 of
74 the original manuscript) plantarflexion moment via the inverse tangent of the ratio of
75 the heel lift to the distance between the head of the fifth metatarsal bone and the
76 potentiometer axis. Our pilot study found this to be in accordance with the motion
77 capture results, with an absolute difference of less than 1.1 degrees in ankle joint
78 angle changes during maximal isometric plantarflexion contractions (from rest to the
79 maximal ankle joint moment; current method: 3.8 ± 1.1 degrees; 2D analysis: $4.9 \pm$
80 1.4 degrees).

81

82 In order to investigate the influence of ankle joint-dynamometer axis misalignment
83 during contractions, which is not accounted for in the current setup, we examined the
84 maximal anterior displacement of the ankle joint axis in our pilot subjects during
85 maximal isometric plantarflexion contractions. The maximal anterior shift of the
86 ankle joint axis during contraction was on average 3.4 ± 2.1 mm, thereby leading to
87 an overestimation of our calculated joint moments. However, relating this anterior
88 shift to the moment arm of the ground reaction force (GRF) acting about the ankle
89 joint, the relative change was approximately 1.7 %. Hence, this drawback has only a
90 negligible effect on our joint moment calculations. Furthermore, the resultant ankle
91 joint moments in the current study were calculated using the vertical component of
92 the GRF, neglecting any force vector direction changes during contraction. Using our

93 pilot data, we compared the maximal ankle joint moments calculated by the vertical
94 component of the GRF to the moments calculated using all three dimensions of the
95 GRF. The maximal ankle joint moment calculated using the vertical component was
96 on average 8% higher compared to the 3D calculations (157.8 ± 47.7 N·m vs. $146.3 \pm$
97 40.9 N·m). However, there was a significant correlation in maximal ankle joint
98 moment between the two methods ($R^2 = 0.996$, $P < 0.01$; see Fig S2) showing that the
99 relative difference between methods was constant, and that calculating the ankle joint
100 moments during isometric contractions using only the vertical component of the GRF
101 is a valid method.
102



115

116 **Fig S2** Relationship between the maximal ankle joint moments measured during a isometric voluntary
117 plantarflexion contraction calculated by talking into account solely the vertical component of the
118 ground reaction force (1D) and by considering the 3D vector of the of the ground reaction force (3D).

119

120 One might argue the fact that we calculated the secant stiffness and not the tangential
121 stiffness of the tendon. Currently the tendon stiffness is determined by the divided
122 change in force by change in elongation from 30-80% of MVC and, thus, only two
123 data points are used to examine the tendon stiffness. However, using the current

124 method, we have a clear steady state in the ultrasound image at target force making
125 digitalization easier than in dynamic contractions, when the tendon deforms quite
126 rapidly during MVC which is in particular problematic when using ultrasound
127 sampling frequencies lower than 30 Hz. By using a constant force held by the subjects
128 for a given time, we may be better able to exclude potential measurement errors due
129 to the ultrasound sampling frequency or small time delays of synchronization between
130 ultrasound and force data when performing ramp contractions. In addition, we were
131 able to negate the effect of loading rate dependency on tendon strain, because the
132 object of interest (in this case a tendon) is given enough time to respond to the applied
133 force (Oberländer et al. 2015). Moreover, before applying the current method we
134 extensively tested this method and compared the calculation of the secant tendon
135 stiffness during sustained contractions with the tangential tendon stiffness during slow
136 and fast isometric ramp contraction and hence using a set of data points digitized over
137 the entire path of the length changes. Although, the stiffness of the tendon is slightly
138 affected by the contraction type, potentially due to the viscoelastic properties of the
139 tendon, we found a similar day-to-day reliability in tendon stiffness between slow
140 ramp contractions and our sustained contraction method, when a skilled and
141 experienced investigator tracked the data points used in the current study (Oberländer
142 et al. 2015).

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144 **References Online Resource**

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